

Ball Aerospace & Technologies Corp.

# External Occulter Planet Finder Mission at L2

## A Potential "Customer" for Robotic Servicing

Charley Noecker (BATC) in collaboration with

University of ColoradoGoddard Space Flight CenterNorthrop Grumman Aerospace SystemsPrinceton University

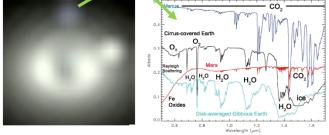
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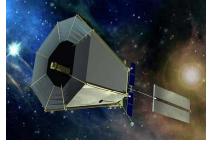
## Terrestrial Planet Finder with Occulters

- The search for planets like Earth, hosting biology like our own
- Three families of instrument concepts
  - Mid-infrared nulling interferometer





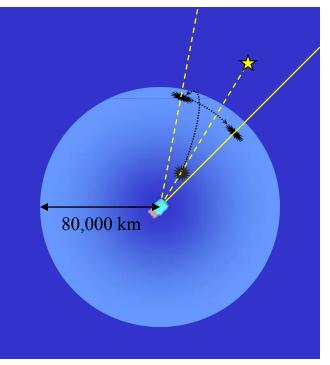
- Visible light coronagraph



- Visible light external occulter
- Occulter is as ancient as blocking the sun's glare with a hand



- Planet-star angle  $< 0.5 \ \mu rad$  and brightness ratio  $\sim 10^{-10}$ .
  - $-\,$  Requires occulter's angular size also  $<0.5~\mu rad$  and shadow depth  ${\sim}10^{-10}$
- Optical diffraction requires a very large occulter, very far away
  - Diameter: 30-100m
  - Separation distance: 30,000-100,000 km
- Move occulter from star to star
  - Typical slew angle between stars is 10-20°
     → 9,000-18,000 km travel
- Seek >120 target observations in 5 years
  → dozens of exoplanets and their spectra





### "Fuel Is Science"

- Science is limited by number of stellar visits in a mission
  - Initial detection Return for characterization
- Visits limited by fuel
  - Typical 1 star/2 weeks for 5 years requires total  $\Delta v \sim 12,000$  m/s
    - High  $I_{sp}$  thrusters needed  $\rightarrow$  fuel mass ~900-1200 kg Xenon
  - Fuel consumed on <u>each slew</u> is proportional to 1/(slew time T):  $\Delta m_{\text{fuel}} = 8 \frac{D}{T} \frac{M_{\text{wet}}}{g \cdot I_{\text{sp}}}$
- Number of stars observed in entire mission depends directly on fuel mass

$$N \cong \underbrace{\begin{array}{c} g \cdot I_{sp} \cdot T_{M} \\ 8 \cdot D \\ 8 \cdot D \\ Typical slew distance between stars \end{array}}^{Mission duration, or time between refuelings}$$

24 March 2010



#### Robotic servicing can extend mission Scenarios with 10 year lifetime

- Option 1: Servicing after 5 years (10 yr total), rendezvous at L2 or at earth-moon L1
  - Doubles number of star observations
- Option 2: Higher fuel rate, servicing every 2 years, rendezvous at L2
  - 60% more stars
- Option 3: Occulter 44% farther from telescope, servicing every 2 years, rendezvous at L2
  - Better science: see planets 20% closer to star
  - More thorough search of each star, and/or
  - Choose candidate stars from 73% larger list

Refueling (recharge Xe tanks)	1200 kg
Replacing thrusters, PPUs	269 kg
Total service, payload to occulter	1469 kg
Number of star observations	250
Number of servicing missions	1

Each service, payload to occulter	1469 kg
Number of star observations	395
Number of servicing visits	4
Total payload to occulter	5876 kg

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Inserviced 10 yr mission expendables: 36,700 kg		
		14(01
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Total payload to occulter

Unserviced 10 yr mission expendables: 36,600 kg

5876 kg



#### Backup Thrusters and Power

- NEXT thruster system (NASA-Glenn)
  - -235 mN,  $I_{sp} = 4100$  s
  - 6.85 kW to thruster
  - 7.25 kW input per Power Processing Unit (PPU)
  - Accelerator electrode life limit estimated at 730 kg Xe
  - With 3 thrusters, estimated mission  $\Delta v=10,193$  m/s

- 3 PPUs and 3 thrusters, cross-strapped
  - Mounted on the outside
  - Total 269 kg
- Power needs
  - Peak power 14.5 kW
  - PPU input 80-160V
- Two 7m Ultraflex arrays
   9 kW each



#### Backup Total Mission Fuel

• Fuel mass fraction is where

$$\frac{m_{\text{fuel}}}{m_{\text{dry}}} = \exp\left(\frac{8 \cdot N^2 \cdot D}{g \cdot I_{\text{sp}} \cdot T_{\text{M}}}\right) -$$

- N is the number of star observations performed in the mission
- $D_1$  is the typical slew distance between 2 stars  $\approx$  (separation distance)\*(typical angle between 2 stars)
- $I_{sp} \approx 4200$  sec is the specific impulse of the thruster and g is 9.8 m/sec<sup>2</sup>
- T<sub>M</sub> is the total mission time, or the time between servicing visits
- For small mass fraction, the science harvest N is

$$N = \sqrt{\frac{g \cdot I_{sp} \cdot T_{M}}{8 \cdot D} \cdot \frac{m_{fuel}}{m_{dry}}} \cdot \left(1 - \frac{1}{4} \cdot \frac{m_{fuel}}{m_{dry}} + O\left(\frac{m_{fuel}^{2}}{m_{dry}^{2}}\right)\right)$$

- We have a mass fraction  $\sim 30\%$ , so the second term is  $\sim 7.5\%$  and the omitted terms are negligible